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Influence of spring characteristics on the behavior of tensegrity mechanisms

Quentin Boehler, Marc Vedrines, Salih Abdelaziz, Philippe Poignet, and Pierre Renaud

Abstract There is today a growing interest for tensegrity mechanisms. Their analysis is however challenging because of their self-stress state. The most popular tensegrity mechanisms use linear springs as tensioned elements. Their synthesis for given user requirements is an open issue. In this article, we propose as a first step to better understand the influence of the spring characteristics, that constitute important design parameters. The influence of spring free length is in particular assessed, considering two planar tensegrity mechanisms. Impact of the spring selection on the workspace, the stiffness and the actuation requirements is observed. The simulation results outline that using nonzero free length springs can be of interest, and conclusions are given on further steps towards a synthesis method.

Key words: tensegrity mechanisms, stiffness computation, workspace estimation.

1 Introduction and scope of the study

Tensegrity systems can be defined [5] as systems in stable self-equilibrated state comprising a discontinuous set of compressed components, *i.e.* struts, inside a continuum of tensioned components, either cables or springs. Thanks to the self-stress state, prestress can be imposed for a same topology in order to modify the level of internal forces. A high stiffness-to-mass ratio can thus be reached. Moreover, since the components are axially loaded, they can be very light and so does the system [7]. Tensegrity mechanisms use actuators to modify their configuration [3, 6]. The tensioned components are then generally linear springs, in order to systematically reach

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equilibrated configurations without tension loss. They have recently received a lot of attention [8, 9, 11], and could be interesting solutions for instance in surgical contexts, where lightweight devices with large workspaces are required [1].

The analysis of tensegrity mechanisms is delicate compared to rigid-body mechanisms. The determination of a mechanism configuration requires for instance to take into account joint variables and external loads while respecting self-equilibrium state conditions. The corresponding static model is obtained using so-called form finding methods [10]. Up to now, related works have been focused on the analysis of tensegrity mechanisms, but not yet on their synthesis. Even the relationship between the design parameters and the mechanism behavior, and the estimation of actuator performances for given specifications remains to be investigated. In this paper, we wish therefore to analyze the sensitivity of the tensegrity characteristics to their design parameters.

The spring characteristics strongly influence the mechanism behavior. We therefore concentrate our efforts on the parameters related to the linear springs used as tensioned components. The influence of spring stiffness is here considered, and more importantly the free length of the springs. To our knowledge, estimating the influence of nonzero free lengths on mechanism performances has not yet been covered in the literature.

As a result, we introduce in this paper an analysis of spring stiffness and free length on the behavior of tensegrity mechanisms. Two planar tensegrity mechanisms of Snelson-cross type [2, 3] are considered, that respectively exhibit 1 and 2-DOF. In section 2, the 1-DOF mechanism is considered. The mechanism is simple enough to allow a detailed analysis of free length influence on mechanism workspace, stiffness and criteria related to actuator requirements, namely actuator stroke, force and energy consumption. In section 3, a 2-DOF mechanism is analyzed. This mechanism can be used as a tool holder in a surgical task [1]. Conclusions are finally given with emphasis on further steps towards a generalization for other tensegrity mechanisms.

2 Sensitivity analysis of a 1-DOF tensegrity mechanism

2.1 Mechanism description

The 1-DOF tensegrity mechanism, based on the Snelson-cross planar tensegrity, is represented in Figure 1. It consists in four nodes $\{A, B, C, D\}$. Two rigid struts of length L connect respectively A with C and B with D . Three linear springs are installed on the outside of the mechanism, with same stiffness k and free length l_0 . An actuator is used to modify the distance $\|AB\| = \rho$, with the node A anchored to the base and B constrained to move in a horizontal direction. In such a situation, the mechanism exhibits 1 DOF, with nodes C and D that have equal vertical displacements. The output variable is defined as y , the Y -coordinate of C and D , and ρ is the input variable. For sake of simplicity, a so-called neutral configuration is defined as

$\|AD\| = \|BC\| = \|CD\| = \rho = 100$ mm with perpendicular struts. It implies that the struts have a length $L = 100\sqrt{2} = 141$ mm.

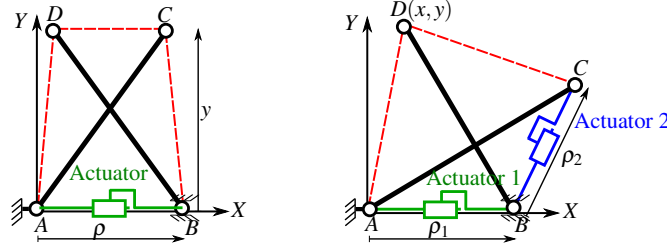


Fig. 1 Kinematic schemes of the 1-DOF (left) and 2-DOF (right) tensegrity mechanisms. In black plain lines, rigid struts and in red dotted lines, linear springs.

2.2 Modeling and analysis criteria

The mechanism modeling consists in deriving expressions of the direct and inverse static models. The output variable y is obtained for a given value of ρ by solving the direct static problem. An energy method, as described in [10], is here considered. The mechanism configuration is then obtained by determining the local minimum of the potential energy U stored in the mechanism springs. In our context, U can be easily computed as

$$U = \frac{1}{2}k(2(l_1 - l_0)^2 + (l_2 - l_0)^2) \quad (1)$$

with $l_1 = \|AD\| = \|BC\|$ and $l_2 = \|CD\|$. The lengths l_1 and l_2 can be expressed using simple geometrical relationships as functions of the variables ρ and y and the length L . In the following, we are only interested in positive solutions of y . The analytic expression of $y = f(\rho)$ is obtained by solving $\frac{\partial U}{\partial y} = 0$ for a given ρ , using a computer algebra system (Mupad, The Mathworks Inc.). Only one admissible solution is found with the simulated conditions where $\rho \in [70, 130]$ mm and $l_0 \in [20, 80]$ mm. The inverse static model that expresses ρ as a function of y is difficult to obtain if nonzero free length of the springs are considered. As noticed previously in [4], the use of nonzero free length springs in a tensegrity mechanism significantly increases its analysis complexity. In our situation, no analytical expression could be found. A numerical approach is then adopted, with a Levenberg-Marquardt algorithm to compute the ρ value for a given y as the solution of $(y - f(\rho))^2 = 0$. The tensegrity mechanism behavior is assessed by using two types of criteria. The first type corresponds to usual mechanism properties, namely the workspace and the stiffness. The workspace is the range of y values for a given range of ρ . The stiffness of the mechanism is defined as $K_y = \frac{\delta F_y}{\delta u_y}$ with δu_y the infinitesimal displacement of nodes C and D along the Y -axis when an infinitesimal external vertical force δF_y is evenly

applied on these nodes, while the actuator is locked. As stated in [2], the stiffness K_y can be estimated with $\frac{\partial^2 U}{\partial y^2}$. The other type of criteria characterizes the actuation requirements of the mechanism. For a predefined path followed by the mechanism in quasistatic conditions, we compute

- $\Delta\rho$: the corresponding required actuator stroke
- \overline{F} and F_{max} : respectively the mean and maximum forces delivered by the actuator
- ΔU : the variation of potential energy.

Meanwhile, the mean value $\overline{K_y}$ and the variation ΔK_y of the stiffness are also estimated. In the presented results, the path is defined as symmetric with respect to the neutral configuration, with a 20-mm displacement. It is discretized in 11 steps to compute the analysis criteria.

2.3 Results and discussion

As it can be observed in Eq. (1), the configuration corresponding to the local minimum of the potential energy U does not depend on the springs stiffness k . The equilibrium configuration is therefore invariant with respect to k . Consequently, modifying the spring stiffness does not modify the mechanism workspace. The mechanism stiffness K_y is proportional to k as it can be observed in Eq. (1). The energy variation ΔU and the actuator force F are also proportional to k . The energy variation corresponds to the energy to be delivered by the actuator. The actuation requirements are therefore linearly dependent on the spring stiffness for a given workspace.

The spring free length l_0 has on the contrary a non-linear influence on the analysis criteria. Figure 2 represents the computation of y and K_y according to l_0 when ρ varies between 70 and 130 mm in 25 steps, for $k = 4$ N/mm. In this example, one may observe that the neutral configuration is not dependent on the spring free length. For a given y , increasing l_0 leads to an increase of K_y while the force delivered by the actuator decreases. This may appear unintuitive, but it is explained by the reconfiguration of the mechanism when l_0 is increased (bottom of Figure 2). The workspace is on the contrary reduced for the same actuation stroke. For given mechanism specifications, interesting compromises therefore exist for nonzero free lengths.

Figure 3 shows the evolution of the criteria related to the actuator requirements. Increasing l_0 leads to the increase of the actuation stroke $\Delta\rho$ while \overline{F} , F_{max} are reduced, as well as the potential energy variation ΔU . An optimal value of l_0 could be searched for in order to adapt the mechanism and the actuator force/displacement characteristics. The influence of the free length on the stiffness is complex, with an increase of the mean value $\overline{K_y}$ but a reduction of the variation ΔK_y . As a conclusion of this case, the analysis suggests first that nonzero free lengths can be of interest for the mechanism performance, and that the choice of l_0 is a compromise between mechanism properties $\overline{K_y}$, ΔK_y and the actuator requirements $\Delta\rho$, \overline{F} , F_{max} and ΔU .

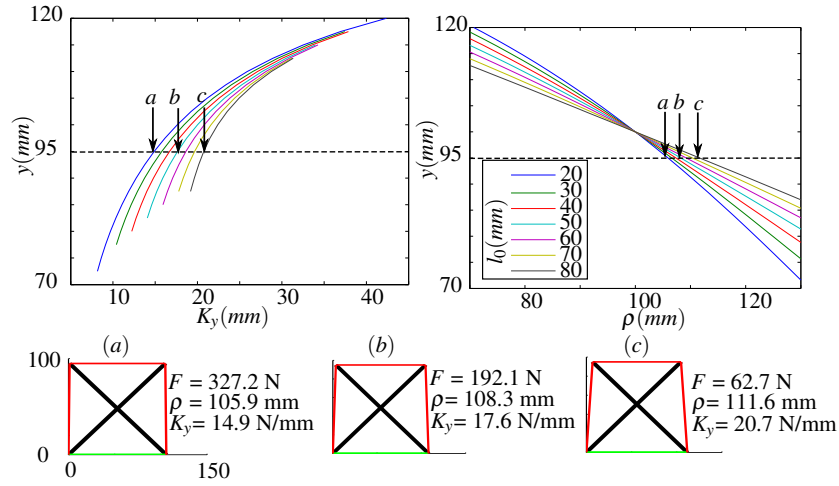


Fig. 2 Relationships between the spring free length l_0 and the stiffness K_y and the workspace. Cases (a), (b) and (c) depict the mechanism at $y=95 \text{ mm}$ for $l_0=20, 50$ and 80 mm respectively.

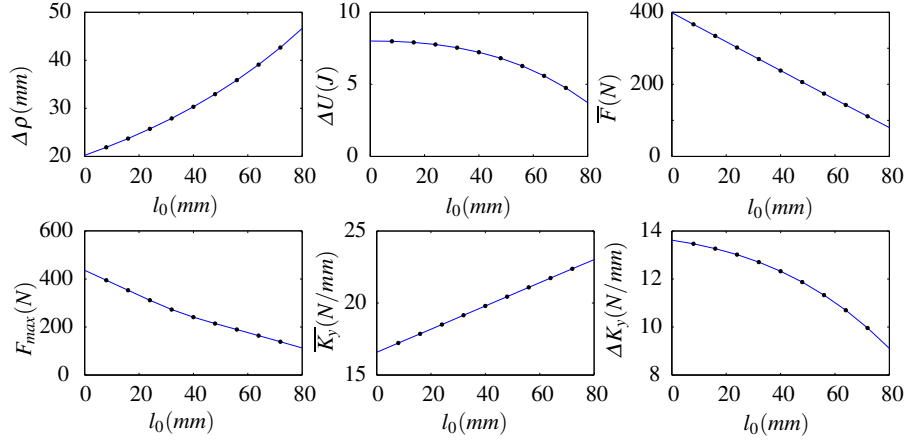


Fig. 3 Evolution of the analysis criteria according to l_0 .

3 Analysis of a 2-DOF tensegrity mechanism

3.1 Mechanism description

A second actuator is integrated between nodes B and C in the previous tensegrity mechanism (Figure 1). The mechanism becomes a 2-DOF manipulator with two joint variables (ρ_1, ρ_2) and its end-effector in D .

3.2 Modeling and analysis criteria

For this 2-DOF mechanism, no analytical direct static model could be obtained if springs have a nonzero free length. Hence, the coordinates of D are determined by minimizing the potential energy U using a Nelder-Mead algorithm. The inverse static model is not implemented since it is not necessary for the evaluation.

Contrary to a rigid-body mechanism, the mechanism configuration does not depend only on (ρ_1, ρ_2) , but also on one parameter that can be either the angle \widehat{ABD} , the variable x , or y . Therefore $U = U_1(\rho_1, \rho_2, x) = U_2(\rho_1, \rho_2, y)$, and the end-effector stiffnesses K_x and K_y in X - and Y -direction can be computed as follows

$$K_x = \frac{\partial^2 U_1(\rho_1, \rho_2, x)}{\partial x^2} \quad (2) \quad K_y = \frac{\partial^2 U_2(\rho_1, \rho_2, y)}{\partial y^2} \quad (3)$$

For this mechanism, analysis criteria are related to the mechanism workspace, stiffness and the actuation requirements:

- A is the area of the reachable workspace
- $\overline{K_x}$ and $\overline{K_y}$ are the mean values of respectively K_x and K_y over the workspace
- ΔK_x and ΔK_y designate the variations of respectively K_x and K_y over the workspace
- \overline{F} and F_{max} are computed as the mean and maximum forces in each actuator.

The workspace is explored with joint ranges that avoid mechanism singularity and loss of tensegrity configuration. A singularity occurs when $\rho_1 = \rho_2 = L/2$, *i.e.* BD is vertical. The lower bounds of ρ_1 and ρ_2 are therefore chosen equal to 75 mm. The strut BD must remain in compression to keep the mechanism in a tensegrity configuration. As a result, the upper bound of the joint variables is such that $\rho_1^2 + \rho_2^2 < 5L^2/2$. A 5-mm step for each joint variable is considered for the computation. The area A is computed by extracting the edge of the discrete set of positions obtained after the exploration of the joint space. With such joint ranges, and thanks to the mechanism symmetry, \overline{F} and F_{max} are the same for both actuators.

3.3 Results and discussion

Similarly to section 2, the influence of the spring stiffness k on the analysis criteria is simple. It does not affect the equilibrium configurations, and linearly impacts the required actuators forces and the stiffnesses.

The variation of K_y is represented in Figure 4, for a spring stiffness $k = 3$ N/mm. For such a mechanism, an end-effector position can sometimes be obtained with two different configurations and hence two different stiffness values. The map is therefore plotted in the joint space. Figure 5 depicts the corresponding reachable workspace. The l_0 value modifies the shape of the workspace boundaries, and the workspace area. In addition, tension losses can occur that limit the workspace, as it can be observed between the middle and right plots of Figure 5. Further analysis shows that the first tension loss takes place when D is at the middle of AC , and

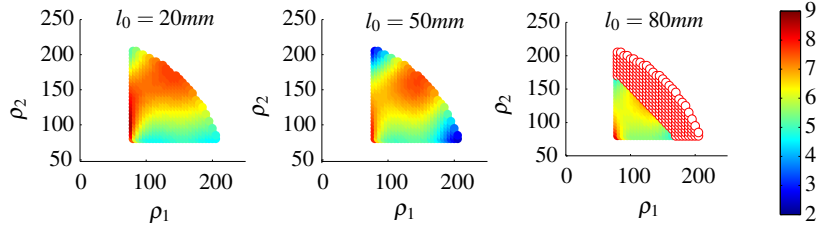


Fig. 4 Variation of the stiffness K_y in N/mm in the joint space for $l_0=20, 50$ and 80 mm. In red circles: unreachable configurations because of tension loss.

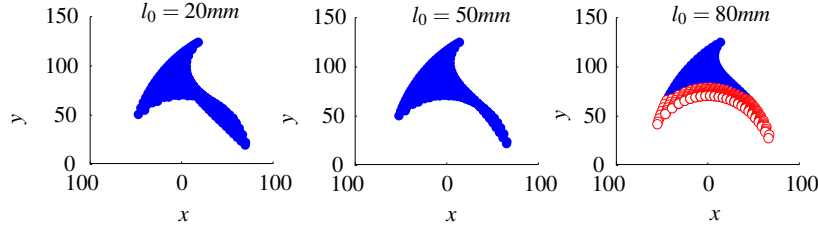


Fig. 5 Reachable workspace for $l_0=20, 50$ and 80 mm. Blue dots: reachable positions / red circles: unreachable positions because of tension loss.

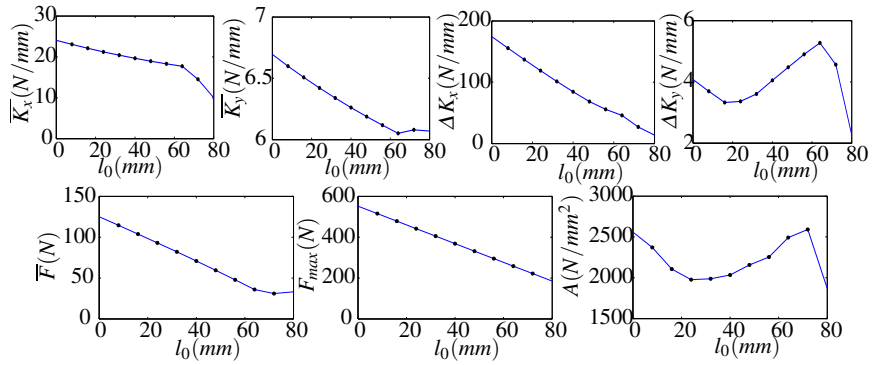


Fig. 6 Evolution of the analysis criteria according to l_0 .

that $l_0 = l_{0 \text{ loss}} = L/2 \simeq 70$ mm. The l_0 value also affects the mean value and the variation of the stiffness over the workspace (left and middle plots of Figure 4).

Figure 6 shows the evolution of the analysis criteria according to l_0 . This evolution of the criteria is notably affected by choosing $l_0 > l_{0 \text{ loss}}$, with in particular a fast reduction of the workspace area A . If $l_0 < l_{0 \text{ loss}}$, $\overline{K_x}$, $\overline{K_y}$, \overline{F} and F_{\max} decrease when l_0 increases. Although ΔK_x is also decreasing monotonously with respect to l_0 , the evolution of ΔK_y is more complex (as it can be seen on Figure 4). The lowest value of ΔK_x is indeed obtained for a nonzero value of l_0 . The evolution of the workspace area A is also non uniform. Increasing l_0 does not necessarily decrease the size of the workspace.

The criteria sensitivity to the free length value is different from the one observed for the 1-DOF mechanism. Increasing l_0 can lead to tension losses, which is quite logical, and affects stiffness and workspace properties. However, the free length can be used to lower the required actuator forces and an adequate choice of l_0 can help increasing the workspace size.

4 Conclusions

In this paper, influence of the spring characteristics on tensegrity mechanisms was considered. Using analysis criteria related to the mechanism properties and the actuator requirements, two planar mechanisms were analyzed. The first major remark is that increasing the free length of the springs can have a beneficial impact on the mechanism or the selection of an adequate mechanism. Whereas the spring stiffness influence can be easily assessed, relationships between the selected criteria and the free length is much more complex. The determination of the spring free length during a mechanism synthesis will need to be performed simultaneously with other design parameters related to the mechanism geometry. The observed significant non-linearities of the sensitivity curves outline also that the selection of the optimization strategy will be delicate, and will be investigated as the next step of this work as well as the generalization for other tensegrity mechanisms.

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