A Framework of Human Impedance recognition
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Abstract—A framework for estimating the human impedance is proposed in this paper. In physical human-robot interaction (pHRI), safety and human acceptance are key issues when humans directly interact with the robots. In order to guarantee the safety and improve performance in pHRI, it is important to estimate the dynamics and intention of the human hand. In this work, we consider that a human subject physically contacts with a force sensor when a haptic device sets force in the proposed framework. The measured force, the surface electromyographic signal and the motion of the hand are used to estimate the parameters of human forearm’s impedance. The effectiveness of the proposed framework is demonstrated by experimental results.

Index Terms—surface electromyographic signal (sEMG), human intention, physical human-robot interaction (pHRI), impedance parameters.

I. INTRODUCTION

Human robot interaction (HRI) is becoming an attractive topic in recent years [1] [2] [3], especially when the human and the robot perform a collaborative task in a common space [4] [5]. In this sense, safety is a key issue which is important to both the robot and human. In general, when a robot interacts a stiff environment [6] or the intention between the robot and the human is different [7] [8], the pHRI system can be unstable.

In order to guarantee the safety of HRI, the dynamics of both the robot and the human hand should be analysed. Researchers have proposed many effective robot control algorithms to achieve a safe HRI [9] [10] [11]. For example, a parameterized dynamical system was employed to allow the robots to adapt their motions to the human intention for physical pHRI (pHRI) in [12]. In [13], in order to achieve seamless pHRI, a human behavior prediction method based on Gaussian Process was presented to estimate human intention.

In this paper, we concentrate on the dynamic analysis of human hand. Considering the human dynamics is closely connected to the muscle activation, we analyse the dynamics of human hand from the perspective of bioinformatics. Recently, electromyography (EMG) signals have been used to analyse the dynamics of human in pHRI. There are many achievements for analysis of human hand dynamics using EMG signals. In [14], a synchronization recognition method of gripping force and posture with respect to EMG signals was proposed to explore the relationship between EMG signal and force. An EMG-based learning method was developed to decode the grasping intention for controlling a robotic assistive device in the early stage of reach-to-grasp motion [15]. In [16], Park et al. proposed a motion intention decoding method based on convolutional neural network with human bio-signals. Wang et al. developed a teaching-learning-prediction model to learn the human demonstrations and to predict human intention in human-robot collaborative tasks [17]. An interactive torque controller based on K-nearest neighbors algorithm by using EMG was presented for an exoskeleton robot to predict the moving direction and to change the behavior of the exoskeleton robot [18]. In [19], a multimodal framework based on EMG and mechanomyogram was developed to recognize the multijoint motion intention of lower limb. In [20], Peternel et al. proposed a human-robot cooperation framework to encode the motion and impedance of human and to provide the feedback of human motor behaviour in real-time. From the above-mentioned algorithm, it can be concluded that the EMG-based method is effective to analyse the dynamics of human hand and to predict the human intention. Inspired by it, we present a neural network method to predict the interactive force between the robot and the human. Based on predicted force, we analyse the impedance parameter of human hand in the process of pHRI. The experimental results will validate the effectiveness of the proposed framework.

The rest of this paper is organized as follows. The proposed method consisting of system framework, data processing and feature selection, force prediction and impedance analysis is presented in Section II. Section III describes experimental results. Finally, conclusion of this paper is presented in Section IV.

II. METHODS

A. System framework

The developed framework is presented in Fig. 1. It consists of three parts: hardware constitution, signal processing, and human intention estimation.
Fig. 1. The proposed system framework.

1) Hardware constitution: This part describes the system’s structure which consists of signal acquisition instrument, haptic device, MYO armband, and control computer. The function of each unit is introduced in the following section and the section of experiment setup.

2) Signal Processing: This part is mainly used to process the collected interaction information such as sEMG signal, interactive force, position/velocity of the endpoint of the human hand. The data preprocessing unit is used for filtering the collected information. The feature selection unit is employed to extract the feature of the sEMG signals and to select proper features.

3) Human intention estimation: In order to estimate human intention, we predict the interactive force and use the predicted results to analyse the variation of impedance in the process of pHRI.

B. Data processing and feature selection

1) Data processing: In this section, we collect the position/velocity of the endpoint of the human hand. Because the human hand moves with the haptic device, the position/velocity can be captured by the haptic device. We collect the sEMG signals of hand by using the MYO armband. Fig. 2 shows the interactive force analysis. We have calibrated the haptic device and have compensated for the gravity of the force sensor with its appendage.

The force analysis of human robot interaction can be represented as

\[ F_h = G + F_{set} \]  

where \( F_{set} \) denotes the set force of the haptic device. \( G \) is the gravity of the force sensor with its appendage. \( F_h \) is the interactive force between the human subject and the haptic device. In this work, \( G = 0 \) N after compensating the the gravity.

The measured force \( F_h \) can be represented as

\[ F_h = [f_x, f_y, f_z]^T \]  

where \( f_x = [f_{x1}, f_{x2}, \ldots, f_{xn}], f_y = [f_{y1}, f_{y2}, f_{yn}], f_z = [f_{z1}, f_{z2}, f_{zn}] \).

2) Feature selection: In order to extract the proper feature of the sEMG signals, we utilize three time domains features (RMS, AR and WL).

The RMS, AR, and WL can be represented as below

\[ f_{rms} = \sqrt{\frac{1}{W_{rms}} \sum_{i=1}^{W_{rms}} n_i^2} \]  

\[ f_{wl} = \frac{1}{W_{wl}} \sum_{i=1}^{W_{wl}} \Delta n_i \]  

\[ f_{ar} = \sum_{i=1}^{p} a_i n_{k-i} + \epsilon_k \]  

where \( W_{i=rms,wl} \) represents the length of moving sampling window. \( n_i \) is the collected sEMG signal. \( a_i \) and \( p \) represent the coefficients and order of AR model, respectively. \( \epsilon_k \) represents the residual white noise.

For convenience, we utilize \( O_I \) to represent the feature of sEMG signals, which is defined as

\[ O_I = [O_1, O_2, \ldots, O_m]^T \]  

where \( O_1 = [o_{11}, o_{12}, \ldots, o_{1n}], O_2 = [o_{21}, o_{22}, \ldots, o_{2n}], \ldots, O_m = [o_{m1}, o_{m2}, \ldots, o_{mn}] \). \( m \) is the number of input channels of sEMG signals and \( n \) is the number of sample data.

By collecting the interactive force and the feature of sEMG signals, the sample data set \( S_{sample} \) can be defined as

\[ S_{sample} = [O_I, F_h]^T \]  

C. Force prediction

In this section, we explore the relationship between the sEMG signal and the interactive force. In the stage of force prediction, we assume that there is a potential relationship of sEMG-force and the schematic diagram is presented in Fig. 3. The process of force prediction is shown in Fig. 4.
Based on the above analysis, we employ a neural network method to predict the interactive force. The framework of neural network can be seen in Fig. 5.

By using the neural network method, the predicted force is presented as

$$\tilde{F} = [Z_1, ..., Z_p, H_1, ..., H_q] W_p^q$$  \hspace{1cm} (8)

where $\tilde{F}$ denotes the predicted force, $Z_i, i = 1, 2, ..., p$ indicates the sum of feature mode, $H_i, i = 1, 2, ..., p$ and $W_p^q$ are the outputs of the enhancement layer and the weight matrix, respectively.

D. Impedance analysis

The impedance of human in the HRI can be expressed as

$$F = K_D P_e + B_D \dot{P}_e + M_D \ddot{P}_e$$  \hspace{1cm} (9)

where $K_D, B_D$ and $M_D$ are the stiffness matrix, the damping matrix and the inertia matrix, respectively. $P_e, \dot{P}_e$ and $\ddot{P}_e$ are the position, velocity and acceleration of human hand. Because the human hand moves with the haptic device, the position/velocity/acceleration can be captured by the haptic device.

In order to analyse the impedance of human hand, a nonlinear least squares method (LSM) is utilized in this paper.

Fig. 6 shows the process of impedance analysis, which consists of two stages: virtual impedance estimation and actual impedance estimation.

- **Virtual impedance estimation**. In this stage, we first to estimate the predicted force by using the proposed neural network method, and then employ LSM method to estimate the virtual impedance parameters based on (9).

- **Actual impedance estimation**. We can directly estimate the actual impedance parameters by collecting the measured interactive force and sEMG signals. By comparing the virtual impedance and actual impedance, we can evaluate the effectiveness of the proposed framework.

### III. RESULTS

A. Experimental setup

To evaluate the performance of the proposed framework, the experimental platform is configured as presented in Fig. 7.

- **Hardware equipment**. The hardware equipment contains Omega 7 (haptic device), the MYO armband, and a FT16498 force sensor.

- **Software environment**. Visual Studio 2013 and MATLAB run on the Window 7 operation system. Universal Serial Bus is used for communication between the force sensor and the control computer. The MYO armband sends the sEMG signals to the control computer by employing Bluetooth technology.

In the process of HRI, the Omega 7 can set the force according to the requirement and can capture the position, velocity and acceleration at the same time. A 3-D printed mounting is used to fix the force sensor. We have calibrated
the force sensor and the Omega 7 to compensate for the influence of its gravity. Therefore, the measured force is the interactive force.

As shown in Fig. 2, a human subject puts his finger to contact the force sensor. When we set a constant downward force for the Omega 7, human hand follows the motion of Omega 7. This system allows the hand to move in a vertical direction. In this process, we capture the sEMG signals, the interactive force and position/velocity/acceleration to estimate the impedance of hand.

B. Feature selection and force prediction

In order to properly select the sEMG feature, we utilize the RMS, AR and WL as the features to estimate the predicted force. Fig. 8 shows the RMS, AR and WL features of sEMG signals.

The predicted forces by using the proposed neural network algorithm are shown in Figs. 9-11. It can be seen that the interactive forces have been accurately predicted.

The error of predicted force by using RMS, AR and WL is presented in Fig. 12. The RMS-based performance achieves minimum error in comparison with that of AR and WL. In order to further evaluate the performance of predicted force with using different features, average error is used in this paper. From Tab. I, the average error for RMS, AR and WL are $3.3906 \times 10^{-6}$ N, $16.453 \times 10^{-6}$ N, and $6.6297 \times 10^{-6}$ N, respectively.

C. Stiffness analysis

In this experiment, we assume that the forces in X and Y directions are zero, so we just perform the experiment in Z-direction. In order to obtain the virtual stiffness, we first estimate the force based on the force prediction algorithm.
Then, the virtual stiffness can be evaluated according to the estimated force and actual position using LSM method. From Fig. 13, it can be seen that the virtual stiffness curves almost overlap with that of actual stiffness. In Fig. 14, it can be seen that the error between virtual stiffness and actual stiffness is very small. In Table II, the values of virtual stiffness and actual stiffness are 11.0890 N/m and 11.0518 N/m, respectively. With these results, it can be concluded that the virtual stiffness can represent the actual stiffness.

IV. CONCLUSION

In this paper, we proposed a novel framework to estimate the impedance of human hand in pHRI. We utilized three features (RMS, AR and WL) to estimate the interactive force and the RMS-based prediction achieved the minimum error. According to the experimental results, the virtual impedance were in accordance with the actual impedance. In this sense, the proposed framework was effective for estimating intention of human hand.
Fig. 12. Error of estimated force by using RMS, AR and WL features.

Fig. 13. Actual and virtual stiffness.

Fig. 14. Error of stiffness.

REFERENCES


